

Chart 8.1 (cont.)

(b) Connections	(c) Load voltage waveforms	(d) Peak forward voltage on SCR	Peak reverse voltage		(g) Max. load voltage ( $\alpha = 0$ ) $E_D = \text{average d-c value}$ $E_D = \text{RMS a-c value}$
			(e) On SCR	(f) On diode	
Single-phase with SCR in series with load		$E$	$E$	$E$	$E_D = \frac{2E}{\pi}$
Single-phase with SCR in parallel with load		$E$	$E$	—	$E_D = \frac{2E}{\pi}$
Single-phase with SCR in series with load and a freewheeling diode		$E$	0	$E$ (CR1 and CR2)	$E_D = \frac{2E}{\pi}$
Three-phase with SCR in series with load		$E$ (possibly $\sqrt{3}E$ if load open and if SCR's have high reverse currents)	$\sqrt{3}E$	$E$	$E_D = \frac{3\sqrt{3}E}{2\pi}$
Three-phase with SCR in series with load		$\sqrt{3}E$	$\sqrt{3}E$	—	$E_D = \frac{3\sqrt{3}E}{2\pi}$
Three-phase with SCR in series with load and a freewheeling diode		$\sqrt{3}E$	$\sqrt{3}E$	$\sqrt{3}E$	$E_D = \frac{3\sqrt{3}E}{\pi}$
Three-phase with SCR in series with load and a freewheeling diode		$\sqrt{3}E$ (1.5E if SCR's shunted by resistance)	$\sqrt{3}E$	$\sqrt{3}E$	$E_D = \frac{3\sqrt{3}E}{\pi}$

(h) Load voltage vs trigger delay angle $\alpha$	(j) Trigger angle full on to full off	Max. steady-state current in SCR		Max. steady-state current in diode rectifier		(p) Ability to pumpback inductive load energy to supply line	(q) Fundamental frequency of load voltage ( $f = \text{supply frequency}$ )	(r) Notes and comments
		(k) Average amp.	(l) Cond. angle	(m) Average amp.	(n) Cond. angle for max. current			
$E_D = \frac{E}{\pi} (1 + \cos \alpha)$	$180^\circ$	$\frac{E}{\pi R}$	$180^\circ$	$\frac{E}{\pi R}$	$180^\circ$	No	$2f$	Diode rectifiers act as free-wheeling path, conduct $(\pi + \alpha)$ degrees with inductive load.
$E_D = \frac{2E}{\pi} \cos \alpha$ (assuming continuous current in load)	$180^\circ$	$\frac{E}{\pi R}$	$180^\circ$	—	—	Yes	$2f$	With resistive load operation is same as circuit (7).
$E_D = \frac{E}{\pi} (1 + \cos \alpha)$	$180^\circ$	$\frac{2E}{\pi R}$	$360^\circ$	$CR_1 = \frac{E}{\pi R}$ $CR_2 = 0.16 \left( \frac{2E}{\pi R} \right)$	$180^\circ$ $148^\circ$	No	$2f$	CR2 necessary when load is not purely resistive. Frequency limited by recovery characteristics of rectifiers and SCR's.
$E_D = \frac{3\sqrt{3}E}{2\pi} \cos \alpha$ ( $0 < \alpha < 30^\circ$ ) $E_D = \frac{3E}{2\pi} [1 + \cos (\alpha + 30^\circ)]$ ( $30^\circ < \alpha < 150^\circ$ )	$150^\circ$	$\frac{\sqrt{3}E}{2\pi R}$	$120^\circ$	$0.16 \left( \frac{3\sqrt{3}E}{2\pi R} \right)$	$134^\circ$	No	$3f$	
$E_D = \frac{3\sqrt{3}E}{2\pi} \cos \alpha$ (assuming continuous current in load)	$150^\circ$	$\frac{\sqrt{3}E}{2\pi R}$	$120^\circ$	—	—	Yes	$3f$	
$E_D = \frac{3\sqrt{3}E}{2\pi} (1 + \cos \alpha)$	$180^\circ$	$\frac{\sqrt{3}E}{\pi R}$	$120^\circ$	$CR_1 = \frac{\sqrt{3}E}{\pi R}$ $CR_2 = 0.14 \left( \frac{3\sqrt{3}E}{\pi R} \right)$	$120^\circ$ $132^\circ$	No	$3f$	Without CR2, SCR's may be unable to turn off an inductive load. Also, CR2 relieves SCR's from free-wheeling duty.
$E_D = \frac{3\sqrt{3}E}{\pi} \cos \alpha$ ( $0 < \alpha < 60^\circ$ ) $E_D = \frac{3\sqrt{3}E}{\pi} \left( 1 + \cos \frac{\alpha}{2} - \frac{\sqrt{3}}{2} \sin \alpha \right)$ ( $60^\circ < \alpha < 120^\circ$ )	$120^\circ$	$\frac{\sqrt{3}E}{\pi R}$	$120^\circ$	$0.056 \left( \frac{3\sqrt{3}E}{\pi R} \right)$	$212^\circ$	No	$6f$	SCR's require two gate signals $60^\circ$ apart each cycle, alternately a gate signal duration $> 60^\circ$ .